

Production of Synthesis Gas with Various Compositions of H<sub>2</sub>, CO,  
and CO<sub>2</sub> from Methanol and Water on a Ni-K/Al<sub>2</sub>O<sub>3</sub> Catalyst

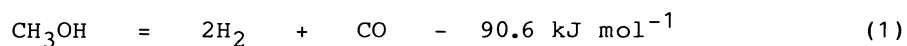
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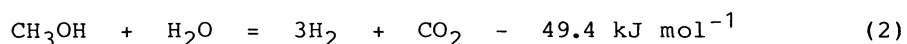
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Mixtures of H<sub>2</sub>, CO, and CO<sub>2</sub> were produced over a Ni-K/Al<sub>2</sub>O<sub>3</sub> catalyst from methanol and water. The composition of the mixtures, in particular the H<sub>2</sub>/CO ratio, was extensively varied by changing reaction conditions such as starting ratio of methanol/water.

There have been several investigations on gasification of methanol over solid catalysts. Decomposition of methanol affords a 2 : 1 mixture of H<sub>2</sub>/CO over various catalysts including nickel and palladium.<sup>1)</sup>



On the other hand, steam reforming of methanol affords a 3 : 1 mixture of H<sub>2</sub>/CO<sub>2</sub> over catalysts containing Cu.<sup>2)</sup>



The combination of these two reactions may result in production of mixtures of H<sub>2</sub>, CO, and CO<sub>2</sub> with various compositions, in particular H<sub>2</sub>/CO ratio, depending on the contribution of each reaction. We report here that the two reactions took place simultaneously on a Ni-K/Al<sub>2</sub>O<sub>3</sub> catalyst, yielding mixtures of H<sub>2</sub>, CO, and CO<sub>2</sub>. The composition of the products was extensively changed by the reaction conditions of reactant CH<sub>3</sub>OH/H<sub>2</sub>O ratio, reaction temperature, and space velocity.

The catalyst was prepared by impregnating aqueous solutions of nickel nitrate and potassium nitrate with extrudate  $\gamma$ -alumina (Ketjen lot no. 6550; 1.5 mm diameter  $\times$  2.4 mm length; BET surface area 260 m<sup>2</sup>g<sup>-1</sup>), followed by drying at 110 °C for 24 h. The loading amounts of nickel and potassium were 4 and 5 mg-atoms(g-Al<sub>2</sub>O<sub>3</sub>)<sup>-1</sup>, respectively. Potassium was effective in eliminating the dehydration reaction of methanol by neutralizing acid sites on the support, and in improving the surface area of metallic nickel on the catalyst.<sup>3)</sup> The catalyst was reduced by flowing methanol at 350 °C for 5 h. The reactions were carried out on a conventional flow system at atmospheric pressure. Mixture of the reactants and balance argon was fed to a tubular-type quartz reactor (26 mm i.d.). Outlet

composition of products and unreacted materials was analyzed on gas chromatographs.

Table 1 shows catalytic activities of Ni-K/Al<sub>2</sub>O<sub>3</sub> in the reaction of methanol and water. In the absence of water the catalyst was active in decomposition of methanol, giving a 2 : 1 molar ratio of H<sub>2</sub> and CO.<sup>3)</sup> Although a slight decrease in methanol conversion was observed in the decomposition with increased pressures, probably due to a poisoning of product CO on the surface,<sup>3,4)</sup> the decomposition obeyed almost zero-order in partial pressure of methanol in the range from 0.3 to 1.0 atm. When water was admitted with methanol, the conversion of methanol was greatly increased. Since the free energy changes in the decomposition and steam reforming reactions are -28 and -49 kJ mol<sup>-1</sup> at 250 °C, respectively, the addition of water makes the reaction thermodynamically more favorable. However, detail mechanism for this enhancement is not clear. Under these conditions, rate of methane formation was negligibly slow (<0.1 mmol h<sup>-1</sup>g<sup>-1</sup>), and neither C<sub>2</sub>-, C<sub>3</sub>-hydrocarbons, HCHO, nor HCOOCH<sub>3</sub> was detected. Most interesting feature of the reaction between methanol and water was that on increasing partial pressure of water, rate of CO formation decreased whereas those of H<sub>2</sub> and CO<sub>2</sub> formation

Table 1. Reaction of CH<sub>3</sub>OH and H<sub>2</sub>O over Ni-K/Al<sub>2</sub>O<sub>3</sub> Catalyst<sup>a)</sup>

Run No.	Partial press. of reactants <sup>b)</sup> /atm		Conversion of CH <sub>3</sub> OH/%	Rate of products formation mmol h <sup>-1</sup> g <sup>-1</sup>			Molar ratio of H <sub>2</sub> /CO
	CH <sub>3</sub> OH	H <sub>2</sub> O		H <sub>2</sub>	CO	CO <sub>2</sub>	
1	1.00	0	15.7	5.8	2.7	0.1	2.1
2	0.50	0	15.2	5.6	2.8	0.1	2.0
3	0.50	0.50	41.2	18.7	2.8	5.0	6.8
4 <sup>c)</sup>	0.50	0.50	92.4	43.2	5.3	11.4	8.1
5	0.30	0	17.4	6.4	3.1	0.1	2.1
6	0.30	0.15	24.5	11.2	3.1	1.7	3.7
7	0.30	0.30	31.3	14.6	2.6	3.1	5.6
8	0.30	0.45	35.5	17.6	2.2	4.2	8.2
9	0.30	0.59	36.1	18.7	1.3	5.3	14.2

a) Catalyst 25 ml (34.1 g), reaction temp 250 °C. b) CH<sub>3</sub>OH feed rate 18.2 + 0.2 mmol h<sup>-1</sup>g<sup>-1</sup>, balance argon. c) Reaction temp 300 °C.

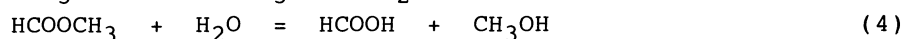
Table 2. Water Gas Shift Reaction over Ni-K/Al<sub>2</sub>O<sub>3</sub> at 250 °C

Partial press. of reactants <sup>a)</sup> /atm		Composition of CO and CO <sub>2</sub> in effluent/%				Rate of CO conversion mmol h <sup>-1</sup> g <sup>-1</sup>
CO	H <sub>2</sub> O	Equilibrium <sup>b)</sup>		Observed		
		CO	CO <sub>2</sub>	CO	CO <sub>2</sub>	
0.09	0.15	1.1	98.9	40.6	59.4	3.62
0.09	0.29	0.4	99.6	0.6	99.4	5.55
0.09	0.44	0.2	99.8	0.2	99.8	5.53
0.09	0.59	0.2	99.8	0.2	99.8	5.60

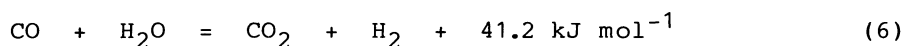
a) Catalyst 25 ml (34.1 g); CO feed rate 5.64 mmol h<sup>-1</sup>g<sup>-1</sup>, balance argon.

b) Equilibrium constant K = 86.92.

increased, giving rise to higher H<sub>2</sub>/CO ratios. The higher ratios were also obtained at elevated temperatures, as exemplified by Run 4 in Table 1. Takahashi et al.<sup>5)</sup> demonstrated two different pathways of the steam reforming reaction. Methanol was converted over a Cu/SiO<sub>2</sub> catalyst to methyl formate and formic acid intermediates, the latter being successively decomposed into final products of CO<sub>2</sub> and H<sub>2</sub>.



However, CO never participates in this mechanism, and in fact only a small amount of CO was observed on the Cu/SiO<sub>2</sub> catalyst even in the absence of water.<sup>5)</sup> By contrast, on a Pt/SiO<sub>2</sub> catalyst was proposed another mechanism, which involves a sequence of methanol decomposition (1) and water gas shift (WGS) reaction (6), though product distribution on changing reactant CH<sub>3</sub>OH/H<sub>2</sub>O ratio was not reported in the literatures.<sup>5,6)</sup>



Since nickel supported on Al<sub>2</sub>O<sub>3</sub> was reported to be active in the WGS reaction,<sup>7)</sup> we have confirmed the reaction on the present catalyst. The results are listed in Table 2. The partial pressure and feed rate of CO in this experiment corresponded to those in the reaction of methanol and water at ca. 30% conversion level. The reaction was extremely rapid and equilibrium compositions were easily obtained with increased partial pressures of water. Therefore, it is most likely that the steam reforming of methanol proceeded through the methanol decomposition and the subsequent WGS reaction.

Another evidence for this pathway comes from

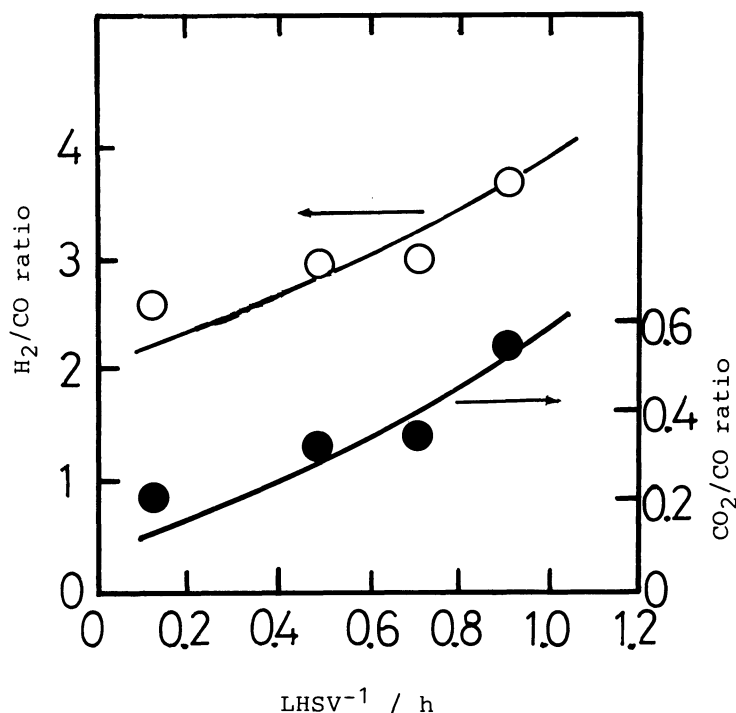


Fig. 1. Change in selectivity of H<sub>2</sub>, CO, and CO<sub>2</sub> as a function of LHSV of methanol in the reaction between methanol and water at 200 °C.

Ni-K/Al<sub>2</sub>O<sub>3</sub> catalyst 12.5 ml (16.3 g),  
reactants methanol/water = 0.30/0.05 atm.

the dependence of product distribution on contact time of the reactants, as illustrated in Fig. 1. When the liquid hourly space velocity (LHSV) was increased, the product ratio of  $H_2/CO$  approached to the value of 2, and that of  $CO_2/CO$  was reduced almost to zero. The conversion of methanol was below 8%, but it increased monotonically with the contact time, i.e. reciprocal of LHSV. This finding indicates that only decomposition of methanol took place at an early stage of the reaction.

As for the reaction of methanol and water shown in Table 1,  $CO_2$  compositions between  $CO$  and  $CO_2$  in the equilibrium are calculated to be more than 96%. However, the effluent compositions did not attain the equilibriums, and rates of  $CO_2$  formation were slower in the reaction of methanol and water than in the WGS reaction. This suggests a competitive adsorption between  $CO$  and reactant methanol on the catalyst, which retarded the WGS reaction (6) rather than the decomposition reaction (1). Thus the composition of  $H_2$ ,  $CO$ , and  $CO_2$  produced from methanol and water, in particular  $H_2/CO$  ratio, may be governed both by the reactions (1) and (6).

In conclusion, mixtures of  $H_2$ ,  $CO$ , and  $CO_2$  with a variety of compositions were selectively produced from methanol and water. The present one-step generation of syn-gas from methanol at lower temperatures is a simple process in which one can obtain a desired ratio of  $H_2/CO$  higher than 2. The compositions may be adapted to many industrial processes, for instance, methanation in which the  $H_2/CO$  ratio of 3 is needed.<sup>8)</sup> Further study including relation between the methanol conversion and the WGS reaction on various catalysts is under investigation.

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